The fracture criticality of crustal rocks

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Accepted 1994 March 17: received 1994 March 13, in original form 1993 November 23

SUMMARY
The shear-wave splitting observed along almost all shear-wave ray paths in the Earth's crust is interpreted as the effects of stress-aligned fluid-filled cracks, microcracks, and preferentially oriented pore space. Once away from the free surface, where open joints and fractures may lead to strong anisotropy of 10 per cent or greater, intact ostensibly unfractured crustal rock exhibits a limited range of shear-wave splitting from about 1.5 to 4.5 per cent differential shear-wave velocity anisotropy. Interpreting this velocity anisotropy as normalized crack densities, a factor of less than two in crack radius covers the range from the minimum 1.5 per cent anisotropy observed in intact rock to the 10 per cent observed in heavily cracked almost disaggregated near-surface rocks.

This narrow range of crack dimensions and the pronounced effect on rock cohesion suggests that there is a state of fracture criticality at some level of anisotropy between 4.5 and 10 per cent marking the boundary between essentially intact, and heavily fractured rock. When the level of fracture criticality is exceeded, cracking is so severe that there is a breakdown in shear strength, the likelihood of progressive fracturing and the dispersal of pore fluids through enhanced permeability. The range of normalized crack dimensions below fracture criticality is so small in intact rock, that any modification to the crack geometry by even minor changes of conditions or minor deformation (particularly in the presence of high pore-fluid pressures) may change rock from being essentially intact (below fracture criticality) to heavily fractured (above fracture criticality). This recognition of the essential compliance of most crustal rocks, and its effect on shear-wave splitting, has implications for monitoring changes in any conditions affecting the rock mass. These include monitoring changes in reservoir evolution during hydrocarbon production and enhanced oil recovery, and in monitoring changes before and after earthquakes, amongst others.

Key words: cracked rock, differential shear-wave anisotropy, fracture criticality, shear-wave splitting.

1 INTRODUCTION
Shear-wave splitting, implying some form of effective elastic anisotropy, has been observed along almost all suitable shear-wave ray paths in at least the uppermost half of the Earth's crust. Such splitting is routinely observed in the shear-wave window above small earthquakes in a very wide range of igneous, metamorphic, and sedimentary rocks in a variety of tectonic regimes, and in reflection surveys, vertical seismic profiles (VSPs), reverse VSPs, and cross-hole surveys in seismic exploration of sedimentary...
basins. Kaneshima (1990) ad Crampin & Lovell (1991) are recent reviews of such observations. The splitting typically displays remarkably similar characteristics despite the wide range of geological and tectonic terrains in which the shear waves propagate. These similarities indicate a common origin of the splitting in the stress-aligned fluid-filled cracks, microcracks, and preferentially oriented pore space present in most rocks. Note that this paper refers to azimuthal anisotropy, where the polarizations of shear-wave splitting vary with azimuth. I do not consider here azimuthal isotropy (transverse isotropy) with a vertical symmetry axis where shear waves invariably split into SV- and SH-wave orientations that may indicate merely that the crust is horizontally layered.

Two characteristics are critical for identifying distributions of cracks (fractures) as the origin of the azimuthal splitting:

1. the horizontal projections of the polarizations of the leading split shear waves are usually parallel or subparallel for all ray paths within the shear-wave window (Crampin & Lovell 1991; see also Booth & Crampin 1985 for a discussion of the shear-wave window).

2. This direction is subparallel to the local direction of maximum horizontal compressional stress in rock volumes where orientations of both polarizations and stress have been reliably determined (Crampin & Evans 1986; Crampin & Lovell 1991).

These characteristics are critical because first, the only anisotropic structure with a large enough solid angle of parallel polarizations at the surface (aperture greater than 70°) is transverse isotropy (hexagonal anisotropic symmetry), or a minor perturbation thereof, oriented so that the symmetry axis is horizontal or subhorizontal (Crampin 1981). Secondly, parallel vertical cracks are the only phenomenon common to all types of crustal rocks that possesses transverse isotropy with a horizontal symmetry axis.

Hydraulic fracturing in the oil industry demonstrates that fluid-filled cracks are usually vertical and strike parallel to the maximum horizontal stress (or strictly, perpendicular to the minimum horizontal stress). In some cases, shear-wave splitting can be plausibly correlated with the presence of large fluid-filled fractures in sedimentary rocks, both directly (Mueller 1991; Lewis, Davis & Vuillermoz 1991), and indirectly (Cliet et al. 1991; Li, Mueller & Crampin 1993). Shear-wave splitting in igneous and metamorphic rocks appears to be the result of cracks and microcracks with diameters less than a few centimetres, possibly much less (Holmes, Crampin & Young 1993). There are also detailed correlations of VSPs with borehole data confirming that shear-wave splitting is associated with aligned cracks (Queen & Rizer 1990; Lefeuvre et al. 1993).

Other important phenomena indicative of cracks are temporal variations in the behaviour of shear-wave splitting before and after earthquakes (Booth et al. 1990; Crampin et al. 1990, 1991; Liu et al. 1993c), and before and after hydraulic pumping (Crampin & Booth 1989). Temporal variations in shear-wave splitting are expected during propagation though distributions of aligned cracks, microcracks, and preferentially oriented pore space known as extensive-dilatancy anisotropy, or EDA (Crampin, Evans & Atkinson 1984; Crampin 1993b). Individual cracks in, what I shall term intact, rock without large fractures are referred to as EDA cracks, since their behaviour can be simulated by distributions of parallel microcracks, even though it is recognized that their individual geometry may include a wide range of aligned structures.

The interpretation of shear-wave splitting as crack-induced anisotropy is dependent on the formalism of Crampin (1978) and Hudson (1980, 1981), who developed expressions for the effective elastic constants of a cracked solid, where crack density is defined as $\varepsilon = N a^3 / V$, $N$ is the number of cracks of radius $a$ in volume $V$ (O’Connell & Budiansky 1974; Hudson 1980, 1981). These formulations assume that, for wavelengths much larger than the crack dimensions, the behaviour of weak distributions of aligned cracks can be modelled by an effective elastic medium with the anisotropic symmetry appropriate for the particular crack distribution. The techniques assume that the cracks
are aligned, small (much less than the seismic wavelength), thin (aspect ratios ≤ 0.1), circular, and isolated (unconnected to other cracks). The formulations appear to be mathematically valid for crack distributions with crack densities of up to about \( \varepsilon = 0.1 \), approximately 10 per cent shear-wave velocity anisotropy (Crampin 1984). With these restrictions, synthetic seismograms calculated through such models simulating cracked rock have been able to match observed three-component seismograms in considerable detail (Bush & Crampin 1991; Liu et al. 1991, 1993a; Slater et al. 1993; Yardley & Crampin 1990).

One of the reasons that effective media simulating flat parallel cracks are such an effective model for synthetic seismograms is that the wavelengths of seismic shear waves typically range from tens of metres to kilometres and are substantially greater than the dimensions of most cracks that are likely to cause the anisotropy (which probably range from a few microns to at most a few metres). This also implies that the elastic anisotropy causing the splitting is insensitive to the dimensions of the cracks. The elastic formulations of Hudson (1981) suggest that attenuation anisotropy is more sensitive to crack dimensions than elastic anisotropy, although up to the present time there is, to my knowledge, only one observation of shear-wave attenuation anisotropy in crustal rocks that has been recognized (Liu et al. 1993a).

The distributions of cracks are also known to be fractal, both in sedimentary (Heffer & Bevan 1990; Yielding, Walsh & Watterson 1992) and igneous and metamorphic rocks (King 1983; Leary 1991; Leary & Abercrombie 1993). Fractal distributions of cracks have two important properties: first, cracks are scale invariant over a wide range of dimensions; and secondly, cracks tend to cluster in space. The scale invariance means that crack distributions contain cracks with a very wide range of dimensions, but because they cluster along the edges of lithologic units, there exist volumes of rock between the larger fractures which only contain cracks of comparatively small dimensions, the EDA cracks.

The reaction of seismic waves to distributions of fractures is determined by the relationship of the fracture dimensions to the seismic wavelengths. Thus, a fractal distribution is divided into two by the seismic wavelength. The reactions to small fractures can be modelled by effective media, whereas the reactions to larger fractures impose specific reflection, transmission, and diffraction effects. This division of the distribution into two will be accentuated by the tendency of small voids to be open and fluid-filled and hence compliant, whereas large fractures will tend to be closed by lithostatic pressure, and consequently less compliant. In addition, fluid-filled cracks with substantial impedance contrasts across the crack face are usually small, whereas large cracks are usually held closed and may be invisible to shear waves unless dilated by hydraulic pumping (Crampin & Booth 1989).

An example of a rock volume with no fractures larger than a metre is the granite batholith of the Underground Research Laboratory of the Atomic Energy of Canada, Ltd, at Pinawa, Manitoba, where there was a comprehensive examination of shear-wave splitting over a wide range of directions (Holmes et al. 1993). In the Mine-by experiment, the rock mass around an advancing test tunnel in a granite batholith, almost completely free of (macro) fractures, was sampled by 4200 Hz shear-wave signals excited on the walls of outer galleries, and recorded at three-component accelerometers in boreholes from the outer galleries, selected to give a good spatial sampling over a range of directions. The path lengths varied from about 7 m to 60 m, and the records displayed shear-wave splitting with observations covering almost 360° of azimuth and 180° of incidence angles. The polarizations match the theoretical polarizations expected of thin penny-shaped microcracks aligned perpendicular to the measured direction of minimum compressional stress some 20° from the vertical, broadly agreeing with the breakout notches in the tunnel itself.

Table 1 lists the percentages of differential shear-wave velocity anisotropy observed in igneous and metamorphic rocks measured (principally) above earthquakes. Differential shear-wave anisotropy is defined as SWA = \( \{ \max (V_{s1}) - \min (V_{s2}) \} / \max (V_{s1}) \times 100 \), where \( V_{s1} \) and \( V_{s2} \) are the velocities of the faster and slower split shear waves, respectively (Crampin 1989). Table 2 lists similar percentages in sedimentary basins from (principally) seismic-exploration investigations. Although neither table is a complete list of all observations, they are all reports known to the author, which provide sufficient information to identify the percentage of shear-wave velocity anisotropy. When only crack density \( \varepsilon \) is reported, \( \varepsilon \times 100 \) has been listed, since this is approximately equal to the percentage of differential shear-wave velocity anisotropy for crack densities less than about 0.1 when the \( V_{p}/V_{s} \) ratio is 1.732 (Crampin 1993a). In two cases, the percentage of shear-wave anisotropy has been inferred from observed P-wave anisotropy, assuming the anisotropy is caused by thin fluid-filled cracks when the differential shear-wave anisotropy is approximately twice the P-wave anisotropy (Crampin 1993a).

The frequencies of the shear waves displaying anisotropy in Tables 1 and 2 cover three orders of magnitude, ranging from about 5 Hz (Graham & Crampin 1993), with wavelengths of over 500 m, to 4200 Hz (Holmes et al. 1993), with wavelengths of about 80 cm. The percentage of anisotropy appears to be independent of frequency, and frequencies are not listed in the tables.

Note that some publications, particularly in exploration seismology, list time delays as measures of anisotropy without giving path lengths or velocities, and it is not always possible to extract percentages of anisotropy or crack densities from the information provided. It would be useful if reports of shear-wave splitting invariably listed crack density, time delays, percentage anisotropy, shear-wave velocity, as well as depth range and the geology in which anisotropy is found.

### 3 OBSERVED ANISOTROPY IN INTACT SUBSURFACE ROCK

Tables 1 and 2 show the wide range of values of differential shear-wave velocity anisotropy observed in a wide range of geological and tectonic conditions. Percentages of anisotropy are listed in order of increasing anisotropy. In order to estimate the anisotropy of intact rock, I attempt to identify values measured near anomalous conditions, such as the
Table 1. Observed percentages of azimuthal differential shear-wave velocity anisotropy in (principally) igneous and metamorphic rocks. Sources of shear waves are earthquakes or natural events unless otherwise specified.

<table>
<thead>
<tr>
<th>Percentage Depth</th>
<th>Rock type / comments</th>
<th>Location</th>
<th>Ref.</th>
</tr>
</thead>
<tbody>
<tr>
<td>anisotropy range (km)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1.42§</td>
<td>&lt;15 Volcanic rocks / aftershocks</td>
<td>Campi Flegrei, Italy</td>
<td>(1)</td>
</tr>
<tr>
<td>1.5</td>
<td>&lt;17 Principally gabbro</td>
<td>Anza, CA, USA</td>
<td>(2)</td>
</tr>
<tr>
<td>2.0</td>
<td>&lt;60 Above subduction zone</td>
<td>Wellington Peninsula, NZ</td>
<td>(3)</td>
</tr>
<tr>
<td>2.0, 2.5</td>
<td>&lt;15 Mixed metam.&amp; sedim. rocks</td>
<td>Los Angeles Basin, CA</td>
<td>(4)</td>
</tr>
<tr>
<td>2.3 ± 1.7</td>
<td>&lt;3.5 Alternative interpret. to (2)</td>
<td>Anza, CA, USA</td>
<td>(5)</td>
</tr>
<tr>
<td>3.0*↑</td>
<td>&lt;0.5 Welded fractured tuff</td>
<td>Tazawako, Akita, Japan</td>
<td>(6)</td>
</tr>
<tr>
<td>3.0@</td>
<td>Unspec.</td>
<td>Unspecified Zone, Can.</td>
<td>(7)</td>
</tr>
<tr>
<td>3.5*</td>
<td>&lt;0.45 Crystalline rock</td>
<td>Mojave Desert, CA, USA</td>
<td>(8)</td>
</tr>
<tr>
<td>&lt;4.0</td>
<td>Metamorphic rocks</td>
<td>W. Deep Levels, S. Africa</td>
<td>(9)</td>
</tr>
<tr>
<td>4.0*</td>
<td>0.4-0.5 Granite/shear-wave sources over 8m-60m raypaths</td>
<td>Manitoba, Canada</td>
<td>(10)</td>
</tr>
<tr>
<td>4.0</td>
<td>&lt;15 Granite and mixed geology</td>
<td>Kinki, Honshu, Japan</td>
<td>(11)</td>
</tr>
<tr>
<td>4.0</td>
<td>&lt;10 Volcanic rocks</td>
<td>Rift zone, Japan</td>
<td>(12)</td>
</tr>
<tr>
<td>4.3</td>
<td>&lt;15 Mixed metam.&amp; sedim. rocks</td>
<td>Los Angeles Basin, CA</td>
<td>(13)</td>
</tr>
<tr>
<td>4.3</td>
<td>&lt;10 Volcanic caldera</td>
<td>Long Valley, CA, USA</td>
<td>(13)</td>
</tr>
<tr>
<td>4.5</td>
<td>&lt;12 Mixed metam.&amp; sedim. rocks</td>
<td>TD, Izmit, Turkey</td>
<td>(14)</td>
</tr>
<tr>
<td>4.5@</td>
<td>&lt;10 Mixed metam.&amp; sedim. rocks</td>
<td>Shikoku, Japan</td>
<td>(15)</td>
</tr>
<tr>
<td>5.0</td>
<td>&lt;10 Volcanic rocks</td>
<td>E.Rift Zone, Hawaii</td>
<td>(16)</td>
</tr>
<tr>
<td>6.0</td>
<td>&lt;2 Volc.&amp; sedim.rocks / geothermal area</td>
<td>Takinoue, Honshu, Japan</td>
<td>(17)</td>
</tr>
<tr>
<td>6.4</td>
<td>&lt;10 Volcanic caldera</td>
<td>Long Valley, CA, USA</td>
<td>(18)</td>
</tr>
<tr>
<td>7.0</td>
<td>&lt;3.1 Volcanic caldera</td>
<td>Phlegrean Fields, Italy</td>
<td>(16)</td>
</tr>
<tr>
<td>7.0§</td>
<td>&lt;20 Metam.rocks / aftershocks</td>
<td>Nahami, NWT, Canada</td>
<td>(19)</td>
</tr>
<tr>
<td>8.0§</td>
<td>&lt; Granite / geothermal area</td>
<td>Cornwall, England</td>
<td>(20)</td>
</tr>
<tr>
<td>9.6</td>
<td>&lt;10 Volc.cald. / resurgent dome</td>
<td>Long Valley, CA, USA</td>
<td>(18)</td>
</tr>
<tr>
<td>10</td>
<td>&lt;30 Principally lower crust</td>
<td>TD, Izmit, Turkey</td>
<td>(21)</td>
</tr>
<tr>
<td>10</td>
<td>&lt;15 Above subduction zone</td>
<td>Wellington Peninsula, NZ</td>
<td>(3)</td>
</tr>
<tr>
<td>10*↑</td>
<td>&lt;1 Granulite facies</td>
<td>Arunta Block, Australia</td>
<td>(22)</td>
</tr>
<tr>
<td>15↑</td>
<td>&lt;10 Volc.caldera / fault zone</td>
<td>Long Valley, CA, USA</td>
<td>(23)</td>
</tr>
<tr>
<td>18↑</td>
<td>&lt;2 Volc.&amp; sedim.rocks / geothermal area</td>
<td>Takinoue, Honshu, Japan</td>
<td>(17)</td>
</tr>
</tbody>
</table>

* shallow (uppermost 1 km);
§ aftershocks;
↑ fault zone;
‡ volcanic rocks;
+ inferred from observed P-wave velocity anisotropy;
© geothermal area of high heat flow;
© estimated; essential information (usually Vs) omitted;

free surface, where larger crack densities and larger crack dimensions might be expected.

The uppermost 1 km of the crust typically has large percentages of anisotropy (marked with asterisks in Tables 1 and 2). Table 2, showing controlled-source measurements in sedimentary rocks where depth ranges are known, shows that particularly large anisotropy is often found in very near-surface rocks (values in uppermost 60 m marked by double asterisks).

Other large percentages of anisotropy can be ascribed to anomalous regions, such as areas of recent deformation as, follows.

(1) Fault zones (Table 1: 15 per cent—Savage, Peppin &
Table 2. Observed percentages of azimuthal differential shear-wave velocity anisotropy in sedimentary rocks. Data from VSPs unless otherwise specified as: RFL—surface-to-surface reflection survey; RFR—surface-to-surface refraction survey; RVSP—reverse VSP; CHS—cross-hole survey; and EQ—earthquake sources.

<table>
<thead>
<tr>
<th>Percentage anisotropy</th>
<th>Depth range (km)</th>
<th>Rock type / comments</th>
<th>Location</th>
<th>Ref.</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.7* - 3.8**</td>
<td>&lt;0.47</td>
<td>Mixed sediments</td>
<td>Devine, TX (1)</td>
<td></td>
</tr>
<tr>
<td>1.4</td>
<td>&lt;0.6</td>
<td>Unspec. sediments / RFL</td>
<td>Pennsylvania, USA (2)</td>
<td></td>
</tr>
<tr>
<td>(1.5,2.0,2.5)®</td>
<td>&lt;2.0</td>
<td>Mixed sediments / RFL</td>
<td>Dimmit, Zavala, and (3)</td>
<td></td>
</tr>
<tr>
<td>1.4*</td>
<td>&lt;0.9</td>
<td>Clay, sandst. &amp; limestone.</td>
<td>Caucasus Basin, Russia (4)</td>
<td></td>
</tr>
<tr>
<td>1.6</td>
<td>1.1 - 2.0</td>
<td>Shale &amp; limestone</td>
<td>Paris Basin, France (5)</td>
<td></td>
</tr>
<tr>
<td>1.0-4.0</td>
<td>&lt;2.4</td>
<td>Mixed sediments / RFL</td>
<td>Silo Field, WY, USA (6)</td>
<td></td>
</tr>
<tr>
<td>-2.0</td>
<td>&lt;3.0</td>
<td>Unspec. sediments / RFL</td>
<td>Unspecified, USA (7)</td>
<td></td>
</tr>
<tr>
<td>24</td>
<td>&lt;2.6</td>
<td>Mixed sediments / RFL</td>
<td>Giddings Fld, TX, USA (8)</td>
<td></td>
</tr>
<tr>
<td>24*</td>
<td>&lt;6</td>
<td>Palaeozoic sedim / EQ</td>
<td>Enola, Arkansas, USA (9)</td>
<td></td>
</tr>
<tr>
<td>2.4*</td>
<td>&lt;1.1</td>
<td>Shale &amp; limestone</td>
<td>Paris Basin, France (5)</td>
<td></td>
</tr>
<tr>
<td>3.0* (3.3, 4.0)® &amp; 7.0*</td>
<td>&lt;1.0</td>
<td>Shales &amp; limestone</td>
<td>Paris Basin, France (10)</td>
<td></td>
</tr>
<tr>
<td>(3.3, 4.0)®</td>
<td>&lt;0.6</td>
<td>Shales &amp; carbonates</td>
<td>Romashkino, Russia (11)</td>
<td></td>
</tr>
<tr>
<td>3.5±0.5</td>
<td>&lt;3.0</td>
<td>Mixed sediments</td>
<td>Dilley, TX, USA (12)</td>
<td></td>
</tr>
<tr>
<td>4*</td>
<td>&lt;0.6</td>
<td>Unspecified sediments</td>
<td>CBTF, OK, USA (13)</td>
<td></td>
</tr>
<tr>
<td>5.0**</td>
<td>&lt;0.06</td>
<td>Bay Mud</td>
<td>San Franc., CA (14)</td>
<td></td>
</tr>
<tr>
<td>7.0*®</td>
<td>&lt;0.64</td>
<td>Unspecified sediments</td>
<td>Lost Hills Field, CA (15)</td>
<td></td>
</tr>
<tr>
<td>&gt;7.0I®</td>
<td>2.5</td>
<td>Fractured chalk</td>
<td>Silo Field, WY, USA (16)</td>
<td></td>
</tr>
<tr>
<td>(7.2, 7.6)†</td>
<td>&lt;0.3</td>
<td>Fault zone</td>
<td>Oroville, CA, USA (17)</td>
<td></td>
</tr>
<tr>
<td>8.0*</td>
<td>&lt;1.4</td>
<td>Fault zone</td>
<td>Parkfield, CA, USA (18)</td>
<td></td>
</tr>
<tr>
<td>9.0*</td>
<td>&lt;0.4</td>
<td>Unspecified sediments</td>
<td>Railroad Gap Field, CA (19)</td>
<td></td>
</tr>
<tr>
<td>10*±</td>
<td>0.8-0.85</td>
<td>Fractured sandstone</td>
<td>S. Casper Creek, WY (20)</td>
<td></td>
</tr>
<tr>
<td>10.5*±</td>
<td>&lt;0.04</td>
<td>Clay &amp; limestone / RVSP</td>
<td>CBTF, OK, USA (21)</td>
<td></td>
</tr>
<tr>
<td>12*±</td>
<td>&lt;0.04</td>
<td>Clay &amp; limestone / CHS</td>
<td>CBTF, OK, USA (22)</td>
<td></td>
</tr>
<tr>
<td>14</td>
<td>&lt;0.47</td>
<td>Sandstone &amp; clay</td>
<td>Livermore, CA, USA (14)</td>
<td></td>
</tr>
<tr>
<td>&gt;30**</td>
<td>&lt;0.01</td>
<td>Unspecified sediments</td>
<td>Cymric Field, CA, USA (19)</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Limestone pavement / RFR</td>
<td>NW England, UK (23)</td>
<td></td>
</tr>
</tbody>
</table>

* shallow (uppermost 1 km); 
** very shallow (uppermost 60 m); 
† fault zone; 
‡ specifically identified large fractures; 
+ inferred from observed P-wave velocity anisotropy; 
® percentage anisotropy correlates with hydrocarbon production; 
@ estimated; essential information (usually Vs) omitted;


Vetter 1990; Table 2: 7.2–7.6 per cent—Leary, Li & Aki 1978; 8 per cent—Daley & McEvilly 1990.

2) Associated with aftershock sequences (Table 1: 7 per cent—Buchbinder 1990), although not all aftershock sequences yield high values (compare Table 1: 1.4 per cent—Iannaccone & Deschamps 1989).

3) Areas where there has been hydraulic pumping, also associated with high heat flow (Table 1: 8 per cent—Roberts & Crampin 1986; 18 per cent—Kaneshima, Ito & Sugihara 1988).

(4) Specific intervals in fractured beds (Table 2: 7 per cent—Lewis et al. 1991; 10 per cent—Shuck 1991).

5) Above subduction zones (Table 1: 10 per cent—Gledhill 1991) where active deformation and high pore-fluid pressures are expected (Prior & Behrmann 1990).

6) Volcanic rocks associated with high heat flow (Table 1: 6 and 18 per cent—Kaneshima et al. 1968; 6.4 and 9.6 per cent—Shib & Meyer 1990; 7 per cent—Savage et al. 1989; 15 per cent—Savage et al. 1990). The 10 per cent of Graham & Crampin (1993), is confined principally to the lower crust,
and is also associated with volcanic rocks and high temperatures.

Excluding values identified as being associated with these special conditions, the range of anisotropy in Table 1 for what may be considered as intact igneous and metamorphic rocks is 1.5 to 4.5 per cent, and the range for intact sedimentary rocks in Table 2 is 1.4 to 3.5 per cent with normalized (approximate) crack densities of $\varepsilon = 0.015$ to 0.045, and $\varepsilon = 0.014$ to 0.035, respectively.

The slightly lower maximum values of anisotropy for intact sedimentary rocks than for intact igneous and metamorphic rocks may have two causes: tectonic stability; and higher $V_p/V_s$ ratios.

1) Many measurements of anisotropy in sedimentary rocks are in stable sedimentary basins where active deformation is less pronounced (although changes due to the sinking or lowering of sedimentary basins may change pore-fluid pressures (Powley 1990) and modify crack densities), whereas measurements in igneous and metamorphic rocks are usually above earthquake sources, where the rocks may be expected to be more heavily deformed and fractured. None of the measurements in Table 2 is reported to be from over-pressurized reservoirs.

2) The value of differential shear-wave anisotropy for a given crack density varies with the $V_p/V_s$ ratio (Crampin 1993a). Thus a crack density of $\varepsilon = 0.05$ has differential shear-wave anisotropy of 5.5 per cent if $V_p/V_s$ is 1.732 (Poisson’s ratio of 0.25, which is frequently assumed for igneous and metamorphic rocks), 4.9 per cent anisotropy for $V_p/V_s$ ratio of 2.5, and 4.6 per cent for $V_p/V_s$ ratio of 3.5.

We see that higher $V_p/V_s$ ratios may account for a large part, but probably not all, of the lower range of percentages of anisotropy in intact sedimentary rocks.

Note that equating percentage anisotropy to $\varepsilon \times 100$ introduces some bias into the estimates of crack density from velocity anisotropy for sedimentary rocks, because of the high $V_p/V_s$ ratio in many sedimentary rocks, which has not been taken into account in obtaining Table 2. Note also that the equivalence of the percentage of differential shear-wave anisotropy to $\varepsilon \times 100$ is a reasonable approximation for small crack densities (Crampin 1993a), but for crack densities greater than about $\varepsilon = 0.1$, displaying more than 10 per cent differential shear-wave anisotropy, there is no simple relationship between the degree of anisotropy and crack density.

4 EQUIVALENT CRACK DISTRIBUTIONS

The crack density $\varepsilon = Na^2/v$ can be normalized to $\varepsilon = a^3$, which represents a distribution of one crack of radius $a$ in each unit cube in a regular distribution of equally sized circular cracks. Since, seismic-velocity anisotropy is insensitive to crack dimensions, as long as the crack size is substantially less than the seismic wavelength, the size of the cracks and the size of the unit cube is not specified. Table 3 lists equivalent values of normalized crack parameters for a range of crack densities giving a range of differential shear-wave anisotropies. Fig. 1 shows schematic illustrations of the density in terms of normalized crack dimensions assuming regular distributions of equally sized circular cracks for the five values of crack density in Table 3, ranging from lightly to heavily cracked rock. Note that it is difficult to accurately represent 3-D distributions in 2-D plane diagrams. The diagrams in Fig. 1 are not average cross-sections but represent the approximate separation of cracks in regular 3-D distributions of equally sized cracks at the relevant crack densities.

Figure 1(a) shows the equivalent crack distributions for a normalized crack density of $\varepsilon = 0.015$ displaying the 1.5 per cent minimum anisotropy observed along ray paths in igneous and metamorphic rocks, or strictly 1.4 per cent in sedimentary rocks (see Tables 1 and 2). Fig. 1(b), for $\varepsilon = 0.045$ displaying 4.5 per cent anisotropy, appears to be the largest anisotropy observed in intact (unfractured) rock, excluding near-surface stress-release anomalies and the particular conditions cited in Section 3, above. The schematic diagrams Figs 1(a) and 1(b) display pervasive cracking, but there is still substantial intact matrix rock between the cracks. I suggest that values of crack density, $0.015 \leq \varepsilon \leq 0.045$, indicate the extent of the cracking in what would otherwise be thought of as intact rock, away from deformations associated with the stress release near the surface and other anomalous volumes within the rock mass.

Figures 1(c), (d), and (e) show distributions for crack densities of $\varepsilon = 0.10$ and greater displaying 10 per cent and larger percentages of anisotropy. Such percentages are only found in rock in the uppermost 1 km, most frequently in the uppermost 60 m (Table 2), or in anomalous regions subsurface as specified in the previous section. The rock is substantially fractured: every crack in Fig. 1(c) for $\varepsilon = 0.1$ is approximately a crack radius from about eight other cracks; Fig. 1(d), where $\varepsilon = 0.125$ and the normalized crack diameter is unity, just spanning the unit cube, is shown for completeness; and Fig. 1(e), for $\varepsilon = 0.42$, crack radius 0.75, shows a very heavily cracked rock.

Clearly, sections of cracks in crustal rocks seldom if ever look like the 2-D illustrations in Fig. 1, and several implicit assumptions have been made to obtain Table 3 and Fig. 1.

(1) It is assumed there are regular distributions of unconnected circular cracks of small, but not necessarily negligible aspect ratio, with dimensions much less than the seismic wavelengths sampling the rock. This may well be a reasonable approximation to the physical reality in uniform unfractured (intact) igneous and metamorphic rocks of low porosity and negligible permeability, as in the Mine-by experiment (Holmes et al. 1993). In sedimentary high-porosity rocks, however, where there is irregular intergranular pore space of significant porosity and permeability, the regular distributions in Fig. 1 are clearly not a good assumption. Nevertheless, shear-wave splitting with very similar characteristics is seen in both low- and high-porosity rocks (Tables 1 and 2; Crampin & Lovell 1991), and there have been several examples of excellent matches of

<table>
<thead>
<tr>
<th>SWA</th>
<th>1.5%</th>
<th>4.5%</th>
<th>10%</th>
<th>&gt;10%</th>
<th>large</th>
</tr>
</thead>
<tbody>
<tr>
<td>$\varepsilon$</td>
<td>0.015</td>
<td>0.045</td>
<td>0.10</td>
<td>0.125</td>
<td>0.42</td>
</tr>
<tr>
<td>$a$</td>
<td>0.25</td>
<td>0.33</td>
<td>0.46</td>
<td>0.50</td>
<td>0.75</td>
</tr>
</tbody>
</table>
There will certainly be a scatter about average (preferred) cracks with coplanar normals is the arithmetic sum of the crack-density weighted mean of the individual polarizations. Of crack distributions in Fig. 1 are likely to give some indication of the relative degrees of alignment even in sedimentary rocks. Consequently, if the scatter about a preferred direction is assumed that the cracks are uniformly aligned. It is assumed that the cracks all have the same dimensions. This is clearly a strong assumption, but because of the good statistical sampling, the schematic illustrations of crack distributions in Fig. 1 are likely to give some indication of the relative degrees of cracking in real rocks.

(3) It is assumed that the cracks are uniformly aligned. There will certainly be a scatter about average (preferred) directions, however, Liu et al. (1993b) demonstrate that, to the first order, the crack density of a combination of parallel cracks with coplanar normals is the arithmetic sum of the cumulative crack densities and the polarization is the crack-density weighted mean of the individual polarizations. Consequently, if the scatter about a preferred direction relative to the stress orientations is comparatively small, as seems likely, the relationships suggested in Fig. 1 will be altered very little by a small range of crack orientations.

(4) Crack densities $\varepsilon \geq 0.1$ (more than 10 per cent shear-wave velocity anisotropy) can only exist if the fluid-pore pressure is sufficiently high to prop open cracks with substantial free faces. Cracks with pore pressures less than lithostatic pressure will tend to close, and closed cracks will tend to heal and become relatively transparent to shear-wave propagation. Large volumes of sedimentary strata with uniformly high pore-fluid pressures are known to exist in the over-pressurized fluid compartments (Powley 1990). High pore-fluid pressures are not as well known in igneous and metamorphic rocks as in sedimentary beds. This may be because there is less reason to sample rocks without hydrocarbons, and even in hydrocarbon reservoirs reliable pore-fluid pressures are difficult to obtain (Powley 1990). It is likely that the much lower overall porosity and lower overall permeability means that high pore-fluid pressures and large crack densities in most igneous and metamorphic rocks exist at least in localized volumes close to the source of the anomaly, such as the stress concentrations associated with fault zones, or in subduction zones where high pore-fluid pressures are known to exist (Prior & Behrmann 1990).

As a consequence of the division of observed values of anisotropy in Tables 1 and 2, I classify cracked rock into intact rock with less than about 4.5 per cent shear-wave anisotropy ($\varepsilon \leq 0.045$) and heavily fractured rock with more than 10 per cent anisotropy ($\varepsilon \geq 0.1$). It is convenient that the formulations of Hudson (1980, 1981) are valid for crack densities of up to about $\varepsilon = 0.1$, the range of crack densities for intact rock (Crampin 1984).

Rocks with shear-wave anisotropy of 10 per cent or greater ($\varepsilon \geq 0.1$) are so heavily fractured that any minor irregularity or disturbance will lead to through going fractures. In particular, the structure of the rock has so little shear strength that the cracked rock mass is unstable to small changes. Note that Hudson (1986) extended his earlier techniques to formally take account of crack-to-crack interactions, but these only make marginal differences to the elastic constants for crack densities less than about $\varepsilon = 0.1$, and in any case heavily fractured disaggregated rock cannot be modelled by effective medium constructs. Intact rock may have minor interconnections between individual cracks, but these will have negligible effects on Hudson's expressions for the long-wavelength limit and their effects on shear-wave propagation, and can be neglected.

5 Fracture Criticality

There is, I suggest, a difference in kind between distributions of cracks in Figs 1(a) and (b), and those in Figs 1(c), (d), and (e). The average crack in Figs 1(a) and (b)
may be considered to be surrounded by largely uncracked rock, whereas, as noted above, for the larger crack densities in Figs 1(c), (d) and (e), an average crack is within a crack radius or less of an average of eight other cracks. Such rock is substantially fractured, as is confirmed by the observed anisotropy listed in Table 2, where larger percentages of anisotropy are only found comparatively near the surface, where stress relief can allow cracks and fractures to be significantly open, or where there are thought to be other known anomalies as listed in Section 3. The normalized crack radii between the minimum 1.5 per cent differential shear-wave anisotropy observed in most otherwise intact subsurface rocks, to the 10 per cent observed in rock near the surface, which is substantially fractured and unstable, differ by a factor less than two (0.46/0.25 = 1.84).

This is a remarkably small range of crack sizes for the large range of rock types sampled and large range of crack dimensions inferred from intact igneous rock (sub-millimetres to millimetres) to unstable fractured rock (metres to many metres). I suggest that this implies there is a value of crack density between \(\varepsilon = 0.045\) and \(\varepsilon = 0.1\) (normalized crack radii 0.33 and 0.46), between the representations in Figs 1(b) and (c), which Crampin & Leary (1993) call fracture criticality, marking the transition from an essentially intact rock to unstable heavily fractured disaggregated rock. The range of normalized crack radii between intact and heavily fractured rock is extraordinarily small, 0.46/0.33 = 1.39. Thus, small increases in crack dimensions can critically alter the significance of the cracking. Any further deformation to the representation in Fig. 1(b) would be likely to lead to pervasive cracking, where the cracks are likely to link up so there can be through-going fracturing, the dispersal of pore fluids through the enhanced permeability, and the loss of shear strength. The small fractures would tend to increase to larger fractures in a fractal relationship in the typical avalanching scenario associated with the phenomenon of self-organized criticality suggested by Bak & Tang (1989).

Once fracture criticality has been exceeded, pore fluids will tend to disperse with a consequent lowering of pore-fluid pressure. The lowering of pore pressure will allow cracks in the rock mass to close (and eventually heal) to crack densities below the level of fracture criticality. The presence of high pore-fluid pressures is expected to have a major effect on the behaviour at fracture criticality. The crack distributions in Figs 1(c), (d) and (e) can only exist in a stable regime if the pore-fluid pressure is sufficient to keep the cracks propped open. This suggests that fracture criticality can only occur in the presence of pore-fluid pressures close to lithostatic pressure.

This suggests that pore-fluid seals have an important influence on the behaviour of rocks undergoing deformation. Thus, it might be expected that the over-pressurized fluid compartments suggested by Powley (1990), where fluid movement is contained by enclosing seals, would be particularly sensitive to changes in conditions acting on the rock mass.

A referee drew my attention to Peacock et al. (1994), published since this paper was submitted, who count crack densities up to 0.4 in cracked marble specimens which have not disintegrated. Photographs of the slides in which these cracks were made show an intersecting network of (randomly oriented) cracks surrounding almost every grain in the slides. This is typical of marble when heated (Rosengren & Jaeger 1968). In such rock fracture criticality has been exceeded, and Rosengren & Jaeger speak of such samples being ‘crumbled with the fingers’. I suggest there are at least two reasons why the specimens have not disaggregated to individual grains. The cracking in the interior of the specimen may not extend to the surface, so that the cracked specimen is held together by a ‘surface tension’ of uncracked or less cracked rock. In addition, the photographs show a minutely irregular interlocking jigsaw-like network of cracks that would not easily pull apart. The 3-D jigsaw of grains is probably the reason that marble shows a gradual rollover above yield strength rather than the brittle failure typical of most rocks (Fredrich, Evans & Wong 1989).

There are also difficulties in the definition of crack density for large values of randomly oriented cracks. The expression for crack density, \(\varepsilon = n a^2/v\), usually refers to weak distributions of flat or nearly flat (strictly elliptical) non-intersecting cracks. Fig. 1 suggests that this definition should to be confined to values of \(\varepsilon\) less than about \(\varepsilon = 0.1\). I suggest it may be reasonable to extend the definition to stronger distributions of parallel non-intersecting cracks as in this paper, which in any case does not rely on any quantitative evaluation above \(\varepsilon = 0.1\), but there are problems in using this definition for larger crack densities when the cracks intersect. Fig. 1 shows that for crack densities above a value of \(\varepsilon = 0.1\), where each crack spans a unit cube, randomly oriented cracks necessarily intersect and the definition for crack density breaks down as the number of cracks is then indeterminate.

6 DISCUSSION

Observations of shear-wave splitting demonstrate that the range of differential shear-wave velocity anisotropy from intact ostensibly unfractured subsurface rock to heavily fractured rock is equivalent to an extraordinarily small range of normalized crack dimensions—compare Figs 1(b) and (c). The behaviour appears to be similar in all rocks traversed by shear waves despite the wide range of porosity, permeability, and internal structure in sedimentary, igneous, and metamorphic rocks. It is argued that this implies that most crustal rocks are so pervaded by fluid-filled cracks that they are close to fracture criticality: the level of cracking marking the transition from what would be thought of as coherent unfractured rock to an unstable disaggregated heavily fractured rock mass. The actual level for fracture criticality would depend on details of pore-fluid pressures and rock type, and geological conditions.

Once fracture criticality has been reached, average cracks would be within a crack radius or less of at least eight other cracks. With such closely spaced cracks, the structure would be weak, and the proximity to this state of fracture criticality implies that most rocks are compliant, where small deformations or changes of conditions may have major effects on the behaviour of the rock mass. Since shear-wave splitting is very sensitive to this internal geometry of the aligned cracks along the ray path, shear waves can be used to monitor the detailed changes to the rock mass.

The results presented here show that some measure of the
proximity to fracture criticality can be estimated from monitoring shear-wave splitting in the rock mass. This means that any situation, where conditions acting on the rock mass change and modify the internal geometry of distributions of cracks in the rock, may be monitored by analysing shear-wave splitting. Since the transition to fracture criticality is likely to be crucial for many processes in the rock mass, and ability to monitor the transition by analysing shear waves may have several applications.

(1) Reservoirs close to fracture criticality are likely to display increased hydrocarbon permeability allowing pore fluids to disperse more easily and thus permit higher rates of production. (Such enhanced permeability is expected to vary with direction and be anisotropic, perhaps strongly anisotropic, which may mean that the behaviour needs to be closely controlled for the full benefits of enhanced permeability to be attained.) There have been several cases reported where the degree of shear-wave anisotropy have been correlated with hydrocarbon production (Cliet et al. 1991; Li et al. 1993), as well cases where higher production has been specifically associated with the presence of large fractures (Mueller 1991; Lewis et al. 1991).

The compliant nature of the rock mass, where small changes in conditions may lead to substantial changes in the behaviour of the rock mass, opens many possibilities. Any situation where rocks are stressed, strained, or otherwise deformed, will modify the internal crack geometry without necessarily leading to fracture criticality, but may still be monitored by analysing shear-wave splitting.

(2) Over-pressurized reservoirs, with fracture criticality and enhanced permeability, are optimum conditions for hydrocarbon production. However, as production proceeds, pore-fluid pressure would decrease locally around the production well and the crack density within that volume would contract to below fracture criticality with the consequent loss of permeability and decline in production probably by encouraging adverse fingering. Consequently, it is desirable to maintain fluid-pore pressures in order to maintain enhanced permeability and enhanced levels of production. These ideas may not be new, but the importance of the results presented here is the recognition that the proximity of fracture criticality and enhanced permeability can be monitored by analysing shear-wave splitting. This opens the possibility of monitoring and possibly even controlling enhanced oil-recovery operations so as to maximize recovery.

(3) The effects of hydraulic fracturing may be predicted and evaluated by analysing shear-wave splitting. Crampin & Booth (1989) identified changes in orientation of shear-wave polarizations induced by hydraulic pumping in a granite batholith.

(4) Changes of stress and strain before earthquakes would be expected to modify crack geometry and change the behaviour of shear-wave splitting. Changes in shear-wave splitting were identified by Peacock et al. (1988) before the North Palm Springs M = 6 earthquake, which were later confirmed by Crampin et al. (1990, 1991). Similar changes have also been reported in less-controlled observations before smaller earthquakes by Booth et al. (1990) and Liu et al. (1993c). These changes could be interpreted as increases in crack aspect ratio (dilatancy) as the stress increases before earthquakes and a decrease in aspect ratio at the time, or in one case (Booth et al. 1990), shortly before the earthquake.

(5) Other sources of seismic anisotropy, such as crystals, may exhibit quite large percentages of shear-wave velocity anisotropy. The demonstration that consistently, almost all examples of percentages greater than about 4.5 per cent, can be associated with rock where heavy fracturing is either directly observed or expected, is further confirmation that the almost universally observed shear-wave splitting in crustal rocks is caused principally by aligned cracks, microcracks, and preferentially oriented pore space.

ACKNOWLEDGMENTS

I thank Peter Leary, Enru Liu and Sergey Zatsepin for many illuminating discussions about crack distributions. This work was partially supported by the Sponsors of the Edinburgh Anisotropy Project, and partially by the Natural Environment Research Council, and is published with the approval of the EAP Sponsors, and the Director of the British Geological Survey (NERC).

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